

## Thermal behavior of 1,3,3-trinitroazetidine

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### Abstract

The thermodynamic parameters of the melting process, the kinetic parameters of the exothermic decomposition and the critical temperature of thermal explosion for 1,3,3-trinitroazetidine (TNAZ) were measured by using a microcalorimeter, a differential scanning calorimeter and a time-to-explosion testing apparatus. Information was obtained on its thermal behavior. © 1997 Elsevier Science B.V.

*Keywords:* DSC; Kinetic and thermodynamic parameters; Microcalorimetry Thermal behavior; TNAZ

### 1. Introduction

1,3,3-trinitroazetidine (TNAZ), which contains one nitramine and one geminal-dinitroalkyl group is a main ingredient of cast explosives. Thermal behavior is one of the most important aspects of TNAZ. There are a few reports on the thermal behavior of TNAZ, such as its initial dissociation mechanism [1] and rapid thermal decomposition process [2–4]. The thermal behavior of TNAZ under non-isothermal TG conditions has also been studied in [2]. However, determination of the thermodynamic parameters of the melting process, the kinetic parameters of exothermic decomposition reaction and the critical temperature of thermal explosion for TNAZ has not yet been reported. The aim of this work is to study these parameters of TNAZ with a microcalorimeter, a differential scanning calorimeter and a time-to-explosion testing apparatus.

### 2. Experimental

#### 2.1. Materials

TNAZ was prepared and purified according to a reported method [5]. The structure of TNAZ was characterized by elemental analysis, molecular weight measurements, IR spectrometry, mass spectrometry and nuclear magnetic resonance spectrometry. Its purity was more than 99.4%.

#### 2.2. Experimental equipment and conditions

The heat flow curves of the melting process of TNAZ were measured with a Calvet microcalorimeter, type E (SETARAM, France), which had a sensitivity of  $66.5 \mu\text{V mW}^{-1}$  and was equipped with two 15 ml vessels. The microcalorimeter was calibrated via the Joule effect. The precision of the enthalpy measurements was 2%. The amount of TNAZ used was about 20 mg.

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DSC experiments were carried out with a MODEL CDR-1 thermal analyzer made in the Shanghai Balance Instrument Factory, using a Ni/Cr-Ni/Si thermocouple plate and working under static air conditions with five different heating rates ranging from 1 to 25 K min<sup>-1</sup>.  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> was used as reference material. The DSC curves of the exothermic decomposition of TNAZ were obtained with a sealed cell of stainless steel. The amount of TNAZ used was about 0.5 mg.

The time-to-explosion experiments for the determination of the critical temperature ( $T_b$ ) of thermal explosion were carried out in measuring equipment for small-scale solid explosives, using empty aluminium blasting cap shells (approximately 7.0 mm O.D.  $\times$  6.1 mm I.D. and 50 mm long). The explosive sample of 40 mg was placed in the shell, which was confined with an aluminium plug and a pressed shim of stainless steel. The sample and confining shell and plug with shim were pressed with an oil press in a suitable die body to a pressure of 4.2 MPa. The above-mentioned assembly was dropped into a preheated Wood's-metal bath, and the time to explosion was measured automatically using a sound responder relay.

### 3. Results and data analysis

#### 3.1. Thermodynamic data for the melting process of TNAZ

A typical heat flow curve of the melting process of TNAZ is shown in Fig. 1. The extrapolated onset temperature ( $T_e$ ), peak temperature ( $T_m$ ), melting enthalpy ( $\Delta H_m$ ) and melting entropy ( $\Delta S_m$ ) obtained by five measurements are  $99.0 \pm 0.1^\circ\text{C}$ ,  $102.5 \pm 0.1^\circ\text{C}$ ,  $30.31 \pm 0.30 \text{ kJ mol}^{-1}$ , and  $80.7 \pm 0.3 \text{ J K}^{-1} \text{ mol}^{-1}$ , respectively. The final temperature of melting ( $T_f$ ) is obtained by the calculated formula presented in Fig. 1. The average value of five measurements is  $99.7 \pm 0.1^\circ\text{C}$ . Thus, the temperature range of melting for TNAZ,  $T_e \sim T_f$  is from  $99.0^\circ\text{C}$  to  $99.7^\circ\text{C}$ .

#### 3.2. The kinetic parameters of thermal decomposition of TNAZ

In order to obtain the kinetic parameters (the apparent activation energy ( $E$ ) and pre-exponential constant

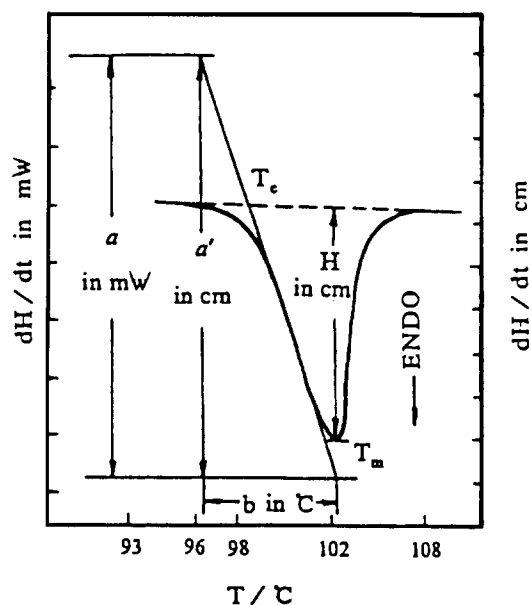


Fig. 1. Typical thermogram of the melting process of TNAZ at a heating rate of  $7^\circ\text{C h}^{-1}$ .  $T_f = T_m - T_{id} = T_m - \text{SHR}_0 = T_m - (H \cdot b)/a'$ , where  $T_{id} = \text{SHR}_0 = (H \cdot b)/a'$ , thermal delay temperature, in  $^\circ\text{C}$ ;  $S = a/a'$ , sensitivity, in  $\text{mW cm}^{-1}$ ;  $H$ , peak height, in cm;  $R_0 = b/a$ , thermal resistance, in  $^\circ\text{C w}^{-1}$ .

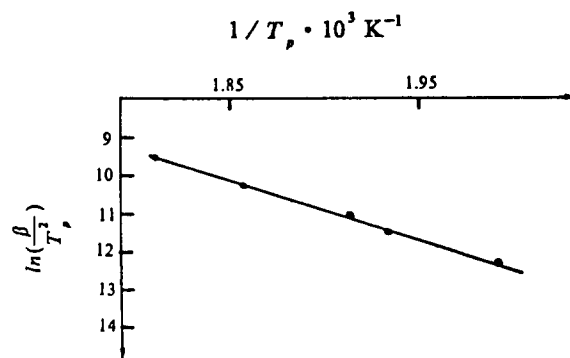


Fig. 2. Kissinger's plot of the exothermic peak temperature obtained by DSC experiments.

(A) of the exothermic decomposition of TNAZ, a multiple heating rate method (Kissinger's method [6]), was employed. As shown in Fig. 2, the relationship between  $\ln(\beta/T_p^2)$  and  $T_p^{-1}$  was a straight line, where  $\beta$  is the heating rate and  $T_p$  is the maximum peak temperature of the exothermic decomposition in the DSC curves. From the original data in Table 1, the apparent activation energy ( $E_K$ ) obtained by Kissin-

Table 1

The values of  $T_e$ ,  $T_{e0}$ ,  $T_p$ ,  $E_K$  and  $T_b$  for TNAZ, HMX and RDX determined from the DSC curves at various heating rates

Sample	$\beta_i/\text{K min}^{-1}$	$T_e/\text{K}$	$T_{e0}/\text{K}$	$T_p/\text{K}$	$E_K/\text{kJ mol}^{-1}$	$T_b/\text{K}$
TNAZ	1.03	—	—	501.7	129.0	511
	2.07	497.7	494.7	512.2		
	5.28	504.7	—	522.1		
	10.5	518.4	—	538.5		
	21.7	528.4	—	552.7		
HMX*	1	537	534.2	538	380.9	541
	5	545	—	548		
	11	550	—	551		
	23	557	—	558		
RDX*	2	473	468.1	485	134.7	482
	5	480	—	497		
	10	490	—	508		
	23	499	—	521		

\*Cited from [8].

ger's method is determined to be  $129.0 \text{ kJ mol}^{-1}$ . The pre-exponential constant is  $10^{10.4} \text{ s}^{-1}$ . The linear correlation coefficient is 0.99. The value of the apparent activation energy ( $E_0$ ) obtained by Ozawa's method [7] is  $130.6 \text{ kJ mol}^{-1}$ . The linear correlation coefficient is 0.99. The value ( $T_{e0}$ ) of the extrapolated onset ( $T_e$ ) corresponding to  $\beta \rightarrow 0$  obtained by Eq. (1) taken from [8] is  $494.7 \text{ K}$ .

$$T_{ei} = T_{e0} + b\beta_i + c\beta_i^2 + d\beta_i^3, \quad i = 1, 2, 3, 4 \quad (1)$$

where  $b$ ,  $c$  and  $d$  are coefficients.

The critical temperature of thermal explosion ( $T_b$ ) obtained from Eq. (2) taken from [8] is  $511 \text{ K}$ .

$$T_b = \frac{E_K - \sqrt{E_K^2 - 4E_KRT_{e0}}}{2R} \quad (2)$$

where  $R$  is the gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ).

For comparing the heat-resistance ability of TNAZ with common simple explosives, the values of  $T_{e0}$  and  $T_b$  of HMX and RDX are also listed in Table 1. This shows that the heat-resistance ability of TNAZ is higher than RDX and lower than HMX.

In order to obtain the values of  $E$  and  $A$  from a single non-isothermal DSC curve, the integral Eq. (3), differential Eq. (4) and exothermic rate Eq. (5) were

employed

$$\ln \left[ \frac{g(\alpha_i)}{T_i - T_0} \right] = \ln \left[ \frac{A}{\beta} \right] - \frac{E}{RT_i} \quad (3)$$

$$\ln \left[ \frac{(d\alpha/dT)_i}{f(\alpha_i)[E(T_i - T_0)/RT_i^2 + 1]} \right] = \ln \left[ \frac{A}{\beta} \right] - \frac{E}{RT_i} \quad (4)$$

$$\ln \left[ \frac{dH_t}{dt} \right]_i = \ln \left\{ AH_0 f(\alpha_i) \left[ 1 + \frac{E}{RT_i} \left( 1 - \frac{T_0}{T_i} \right) \right] \right\} - \frac{E}{RT_i} \quad (5)$$

where  $g(\alpha)$  is the integral mechanism function,  $T_i$  is the temperature (K) at time  $t$ ;  $T_0$  is the initial point at which DSC curve deviates from the baseline;  $R$  is the gas constant;  $\alpha$  is the conversion degree;  $f(\alpha)$  is differential mechanism function;  $dH_t/dt$  is the exothermic rate at time  $t$ ;  $H_0$  is total exothermicity of the substance (corresponding to the global area under the DSC curve);  $H_t$  is the reaction heat in a certain time (corresponding to the partial area under the DSC curve).

The original data tabulated in Table 2 were fitted to the integral, differential and exothermic rate Eqs. (3)–(5) by linear least-squares, iterative, combined dichotomous and least-squares methods [9]. The calculated results of  $E$  and  $A$  are shown in Table 3. The values of  $E$  and  $A$  obtained from a single non-isothermal DSC curve are in good agreement with the calculated values

Table 2  
Data of TNAZ determined by DSC with the sealed cell of stainless steel

Data point	$T_i/\text{K}$	$\alpha_i$	$(dH_i/dt)_i/\text{mJ s}^{-1}$	$(d\alpha/dT)_i \times 10^4/\text{K}^{-1}$
1	484.40	0.0093	0.0975	2.582
2	487.65	0.0174	0.1389	3.680
3	490.90	0.0314	0.1481	3.923
4	494.90	0.0453	0.1519	4.023
5	497.65	0.0587	0.1544	4.090
6	501.65	0.0749	0.1736	4.600
7	505.90	0.0935	0.1833	4.855
8	510.15	0.1133	0.2155	5.708
9	514.15	0.1365	0.2711	7.182
10	518.40	0.1688	0.3644	9.654
11	521.15	0.2069	0.5130	13.59
12	525.40	0.2667	0.7004	18.55
13	530.15	0.3608	1.0598	28.07
14	534.90	0.4828	1.4548	38.54
15	538.40	0.6403	1.8067	47.86

$T_0 = 479.65 \text{ K}$ ;  $H_0 = 2160 \text{ mJ}$ ;  $\beta = 0.1748^\circ\text{C s}^{-1}$ .

Table 3  
Calculated values of kinetic parameters of thermal decomposition for TNAZ

Eq. (3)		Eq. (4)		Eq. (5)	
$E/\text{kJ mol}^{-1}$	$\log A/\text{s}^{-1}$	$E/\text{kJ mol}^{-1}$	$\log A/\text{s}^{-1}$	$E/\text{kJ mol}^{-1}$	$\log A/\text{s}^{-1}$
132	9.9	139	9.7	135	9.1

obtained by the methods of Kissinger and Ozawa. Thus, the values of  $E$  of  $133 \text{ kJ mol}^{-1}$  and  $A$  of  $10^{9.8} \text{ s}^{-1}$  are believed to be for the thermal decomposition of TNAZ.

### 3.3. The critical temperature of thermal explosion of TNAZ

The relationship between the thermal explosion temperature ( $T_b$ ) and the determined explosion induction time ( $t_{\text{exp}}$ ) obtained using the critical temperature measured for thermal explosion of small-scale solid explosives is shown in Fig. 3.

The value of critical temperature of thermal explosion ( $T_b$ ), i.e. the value of  $T_1$  corresponding to  $t_{\text{exp}} = 1000 \text{ s}$  obtained from Fig. 3 is  $523 \text{ K}$ , which is agreement with the value of  $T_b$  of  $511 \text{ K}$  obtained using Eq. (2) for estimating the critical temperature of thermal explosion under non-isothermal DSC conditions. The error between the experimental and calculated values is estimated to be 2.3%.

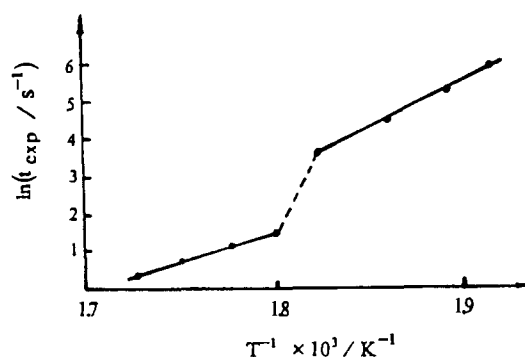


Fig. 3. Explosion time of TNAZ.

## 4. Conclusions

1. The extrapolated onset temperature, peak temperature, melting enthalpy and melting entropy of the melting process of TNAZ are  $99.0 \pm 0.1^\circ\text{C}$ ,  $102.3 \pm 0.1^\circ\text{C}$ ,  $30.31 \pm 0.30 \text{ kJ mol}^{-1}$  and  $80.7 \pm 0.3 \text{ J K}^{-1} \text{ mol}^{-1}$ , respectively. The melting temperature range is from  $99.0^\circ\text{C}$  to  $99.7^\circ\text{C}$ .

2. The apparent activation energy and pre-exponential constant of the exothermic decomposition of TNAZ are  $133 \text{ kJ mol}^{-1}$  and  $10^{9.8} \text{ s}^{-1}$ , respectively.
3. The values of critical temperature of thermal explosion of TNAZ obtained by using a time-to-explosion testing apparatus and the non-isothermal DSC are 523 and 511 K, respectively.
4. The heat-resistance ability of TNAZ is higher than RDX and lower than HMX.

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